

Turbulence wave number spectra reconstruction using radial correlation reflectometry

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Fluctuation reflectometry is widely used technique providing information on the tokamak plasma micro turbulence. Technical simplicity and operation at a single access to plasma are among its merits, which however cause interpretation problems related to localization of measurements and wave number resolution. In order to improve the fluctuation reflectometry wave number selectivity a more sophisticated radial correlation reflectometry (RCR), using simultaneously different frequencies for probing was proposed and developed at numerous magnetic fusion devices. The coherence decay of two scattering signals with growing difference of probing frequencies is studied in this diagnostic and applied for estimation of the turbulence radial correlation length in a very straightforward manner. Namely, it is assumed that the distance between cut offs at which the correlation of two reflectometry signals is suppressed is equal to the turbulence correlation length.

However already in 1D numerical Born approximation analysis [1] a role of small angle scattering was shown, reducing the diagnostic spatial resolution and leading to a very slow decay of coherence in RCR. This effect was confirmed in RCR linear analytic theory in 1D and 2D model [2, 3], by 1D full-wave modeling [4] and 2D Born approximation computations [5] thus appealing for a more sophisticated RCR data interpretation.

In the present paper an analytical integral formula expressing the RCR cross-correlation function (CCF) in terms of turbulence radial wave number spectrum is analyzed and a procedure of its correct inversion for the spectrum determination from the CCF is proposed. The feasibility of this spectrum reconstruction procedure is confirmed in 1D numerical modeling performed both in linear approximation and using the full-wave approach.

The turbulence wave number spectrum reconstruction background.

We treat the RCR problem using 1D model describing the O-mode probing by equation

$$\left\{ \frac{d^2}{dx^2} + \frac{\omega^2}{c^2} - \frac{4\pi e^2 [n(x) + \delta n(x)]}{m_e c^2} \right\} E_z(x, \omega) = 0, \quad (1)$$

where $n(x) = n_c(\omega_1)x/x_c(\omega_1)$ is the background density profile supposed linear in this paper and $\delta n(x)$ stands for turbulent fluctuations assumed statistically homogeneous. In the

analytical section we suppose the transparent plasma size $x_c(\omega_1)$ and the turbulence correlation length l_c to be large enough to treat (1) in the WKB approximation. The corresponding solution takes a form of incident and reflected wave superposition

$$E = 2E_0 \left[1 - \frac{n(x) + \delta n(x)}{n_c(\omega)} \right]^{1/4} \exp \left[i \int_0^{x_c} \frac{\omega}{c} \sqrt{1 - \frac{n(x) + \delta n(x)}{n_c(\omega)}} dx \right] \cos \left[\int_{x_c}^x \frac{\omega}{c} \sqrt{1 - \frac{n(x') + \delta n(x')}{n_c(\omega)}} dx' + \frac{\pi}{4} \right] \quad (2)$$

In the case the turbulence level is low enough, so that the reflected wave phase perturbations are small $\delta\varphi(\omega) = \frac{\omega}{c} \int_0^{x_c} \frac{\delta n(x)}{n_c(\omega)} \frac{dx}{\sqrt{1 - n(x)/n_c(\omega)}} < 1$, the fluctuation reflectometry signal is given by

simple expression $\delta E = i\delta\varphi(\omega)E_0 \exp[i\varphi_0(\omega)]$; ($\varphi_0(\omega) = 2 \int_0^{x_c} \frac{\omega}{c} \sqrt{1 - \frac{n(x)}{n_c(\omega)}} dx$). Correspondingly, the

RCR CCF is proportional to the phase perturbation correlation function, which may be expressed in terms of the turbulence wave number spectrum [2]. Finally the CCF takes a form

$$CCF = 4 \frac{\omega_1^2 x_c(\omega_1)}{c^2} \cdot \frac{\delta n^2}{n_c^2(\omega_1)} \int \frac{d\kappa}{2\pi} \frac{\tilde{n}_\kappa^2}{|\kappa|} e^{i\kappa\Delta} F[\sqrt{\kappa x_c(\omega_2)}] F^*[\sqrt{\kappa x_c(\omega_1)}] |E_0|^2 \exp[i(\varphi_0(\omega_2) - \varphi_0(\omega_1))] \quad (3)$$

where $\Delta = x_c(\omega_1) - x_c(\omega_2)$ is the cut-off separation, δn^2 determines the density perturbation level, $F(s) = \int_0^s \exp(i\zeta^2) d\zeta$ is a Fresnel integral and the spectrum \tilde{n}_κ^2 is related to the density fluctuation correlation function by expression $2\pi \langle \delta n(x') \delta n(x'') \rangle = \delta n^2 \int_{-\infty}^{\infty} \tilde{n}_\kappa^2 \exp[i\kappa(x' - x'')] d\kappa$.

The $1/\kappa$ factor entering the integral in (3) is responsible for underlining the contribution of small angle scattering off long scale fluctuations into the RCR signal. This singularity saturated only for $\kappa x_c < 1$ due to the Fresnel integral behavior ($F(s) \approx s$ at $s \ll 1$) leads to a very slow decrease of CCF mentioned above that complicates the RCR data interpretation. The way to exclude this singularity and reconstruct the turbulence wave number spectrum is provided by the similarity of (3) and Fourier transform. Namely, it is possible to show that the relation inverse to (3) expressing the turbulence spectrum in terms of CCF takes a form

$$\frac{\delta n^2}{n_c^2(\omega_2)} \tilde{n}_\kappa^2 = \frac{\sqrt{i}}{2\sqrt{\pi}} \frac{c^2}{x_c(\omega_2) \omega_2^2} \frac{|\kappa|}{F[\sqrt{\kappa x_c(\omega_2)}]} \int CCF e^{-i\kappa\Delta} d\Delta \quad (4)$$

Numerical reconstruction of the turbulence spectrum and CCF.

Here we shall analyze the accuracy of this inversion using the CCF computed numerically from (1) in the frame of full-wave modeling or Born approximation (the scattered signal in

this case is given by expression $A_s = \frac{i\omega\sqrt{S_i}}{16\pi} \int_0^\infty \frac{\delta n(x)}{n_c} E_0^2(x) dx$ where electric field $E_0(x)$ is normalized to unite power flux density). In the later case the superposition of $m=10^5$ harmonics $\delta n(x) = \delta n_0 \sum_{j=1}^{j=m} \cos(jqx + \varphi_j) \sqrt{\frac{2q}{\pi} \tilde{n}_{jq}^2}$ possessing wave numbers jq , random phases φ_j , and amplitude distributed in accordance with the turbulence spectrum \tilde{n}_κ^2 is used in analysis. The calculation parameters are as follows: $x_c = 40cm$; correlation length $l_c = 2cm$;

$\omega_1 = 6 \cdot 10^{11} \text{ c}^{-1}$ The averaging is performed over ensemble of typically 500 random phase samples. In the case of spectrum $\tilde{n}_k^2 = \sqrt{\pi} l_c e^{-l_c^2 k^2 / 4}$, shown in fig. 1a by red curve, the CCF calculated in the interval $-20l_c < \Delta < 20l_c$ is shown in fig. 1b by the black curve. It is much broader than turbulence Gaussian correlation function (red curve in fig. 1b), asymmetric and

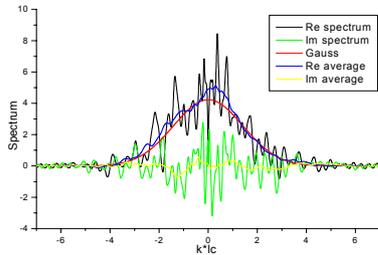


Fig. 1a. The spectrum versus normalized wave number.

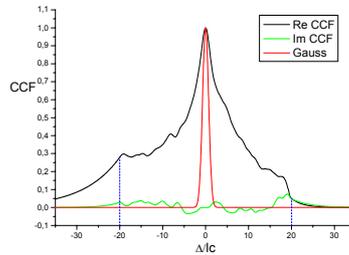


Fig. 1b. The signal and turbulence CCF.

possesses small, but finite imaginary part, shown by green line. As it is obvious, the CCF provides no information on the turbulence correlation function. Accordingly, the CCF spectrum obtained after extrapolation of the CCF to higher Δ values is very peaked around the zero wave number, unlike the initial Gaussian spectrum. However after been treated in agreement with (4) its real part takes a form similar to the Gaussian (see fig. 1a). The oscillations of the reconstructed real part of the spectrum around the Gaussian one are produced by discontinuities of the extrapolation procedure at $\Delta = \pm 20l_c$. A smaller imaginary part of the reconstructed spectrum (shown by green line in fig. 1a) is oscillating around the zero line. Smoothing of these oscillations by integrating over a wave number interval results in a spectrum similar to Gaussian and possessing very small imaginary part, as it is shown in fig. 1a. It is important to note that these oscillations originated by extrapolation procedure could be removed to the matching region $\Delta = \pm 20l_c$ by performing Fourier transform of the reconstructed spectrum providing the turbulence CCF. The result of this transformation in the case of spectrum of fig. 1a is shown in fig. 2a. As it is seen there, the reconstructed real part of the turbulence CCF fits perfectly the initial Gaussian correlator at $\Delta < 2l_c$. The finite value of the CCF imaginary part, as well as CCF random behavior at $\Delta > 2l_c$ should be attributed to imperfect averaging. As it is seen in fig. 2b, the level of the reconstructed CCF imaginary part as well as its real part at $\Delta > 2l_c$ is suppressed by increasing the averaging ensemble from 500 to 1000 samples. Using the approach based on relation (4) we have also reconstructed a multi

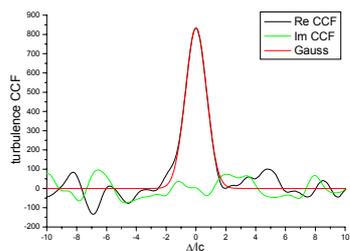


Fig. 2a. The turbulence CCF.

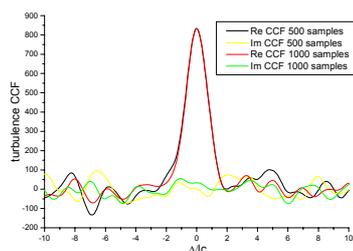


Fig. 2b. The turbulence CCF.

component spectrum shown in fig. 3a by red curve. The corresponding turbulence CCF shown in fig. 3b by red curve possesses a typical oscillatory structure. The

RCR CCF real part shown there by the blue curve is very different from the original one, however application of the reconstruction procedure based on (4) results in complex spectrum, real part of which fits well the original turbulence spectrum even without smoothing, whereas the imaginary one oscillates around zero and is removed by smoothing. The Fourier transform of the obtained spectrum results in the perfect turbulence CCF

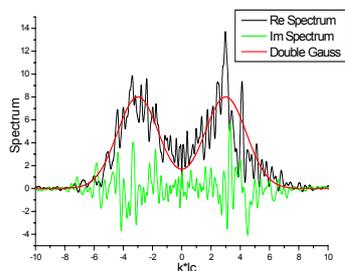


Fig. 3a. The turbulence spectrum.

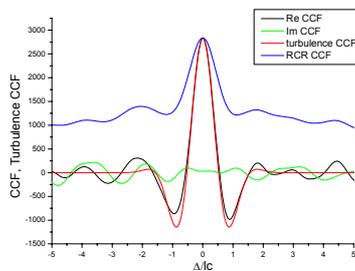


Fig. 3b. The turbulence CCF.

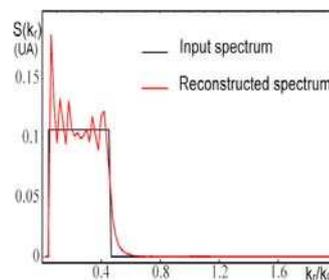


Fig. 4. The turbulence spectrum.

reconstruction, as it is shown in fig. 3b. The application of the developed procedure to the full-wave modeling of (1) using the numerical scheme described in [4] and following parameters: $x_c = 20cm$; $l_c = 0.25cm$; $\omega_1 = 1.9 \cdot 10^{11} c^{-1}$ also resulted in successful reconstruction of rectangular turbulence spectrum in spite of correlation length been smaller than the probing wavelength, as it is seen in fig. 4.

Conclusion.

Concluding it is worth to underline that application of the proposed procedure to the turbulence spectrum and CCF reconstruction from the RCR data in numerical modeling have led to very promising results. The demonstrated possibility of fine reconstruction, at least in 1D geometry, is proving the procedure feasibility and appealing for further optimization and tests in 2D numerical modeling.

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